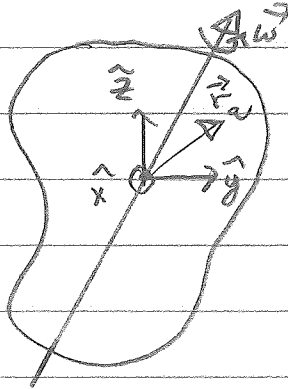


Lecture #10: Principal Axes

Origin of coordinates on axis of rotation.



$$\vec{L}_{\text{rot}} = \sum_a m_a \vec{r}_a \times \vec{v}_a = \sum_a m_a \vec{r}_a \times (\vec{\omega} \times \vec{r}_a)$$

with $\vec{A} \times (\vec{B} \times \vec{A}) = A^2 \vec{B} - \vec{A} (\vec{A} \cdot \vec{B})$ identity

$$\vec{L} = \sum_a m_a \left[r_a^2 \vec{\omega} - \vec{r}_a (\vec{\omega} \cdot \vec{r}_a) \right]$$

$$L_i = \sum_a m_a \left[r_a^2 \omega_i - r_{a_i} \sum_j \omega_j r_{a_j} \right]$$

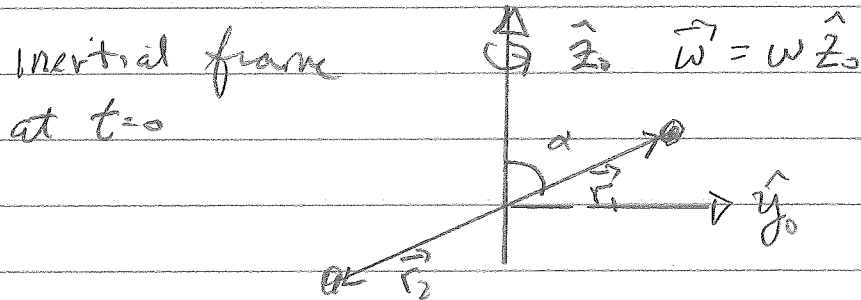
$$= \sum_j \omega_j \left[\sum_a m_a (r_a^2 \delta_{ij} - r_{a_i} r_{a_j}) \right]$$

$$= \sum_j I_{ij} \omega_j$$

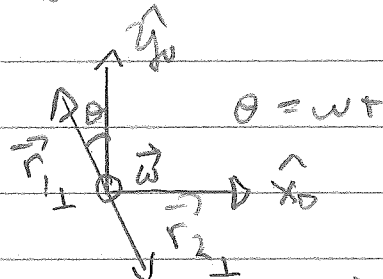
$$\vec{L} = \vec{I} \cdot \vec{\omega}$$

$\vec{L}, \vec{\omega}$ not necessarily parallel

Example: rotated dumbbell (2 masses m connected by rigid, massless rod of length l)



looking down \hat{z}_0 axis:



$$\vec{r}_{1\perp} = \frac{l}{2} S_\alpha (\cos \omega t \hat{y}_0 - \sin \omega t \hat{x}_0) \quad S_\alpha \equiv \sin \alpha$$

$$\vec{r}_{2\perp} = \frac{l}{2} S_\alpha (-\cos \omega t \hat{y}_0 + \sin \omega t \hat{x}_0)$$

$$\vec{L} = \sum_{a=1}^2 m \vec{r}_a \times \dot{\vec{r}}_a \quad (\text{with } S_\pm = \sin \omega t, C_\pm = \cos \omega t)$$

$$\vec{r}_1 \times \dot{\vec{r}}_1 = \frac{l^2 \omega}{4} (S_\alpha C_+ \hat{y}_0 - S_\alpha S_+ \hat{x}_0 + C_\alpha \hat{z}_0) \times (-S_\alpha S_+ \hat{y}_0 - S_\alpha C_+ \hat{x}_0)$$

$$= \frac{l^2 \omega}{4} \left[+S_\alpha^2 C_+^2 \hat{z}_0 + S_\alpha^2 S_+^2 \hat{z}_0 + S_\alpha C_+ S_+ \hat{x}_0 + S_\alpha C_+ C_+ \hat{y}_0 \right]$$

$$= \frac{l^2 \omega}{4} \left[S_\alpha^2 \hat{z}_0 + S_\alpha C_\alpha (S_+ \hat{x}_0 - C_+ \hat{y}_0) \right]$$

2nd mass gives same, so

$$L_{z_0} = \left(\frac{m\omega l^2}{2} \right) S_\alpha^2$$

$$L_{x_0} = \left(\frac{m\omega l^2}{2} \right) S_\alpha C_\alpha \sin \omega t$$

$$L_{y_0} = \left(\frac{m\omega l^2}{2} \right) S_\alpha C_\alpha (-\cos \omega t)$$

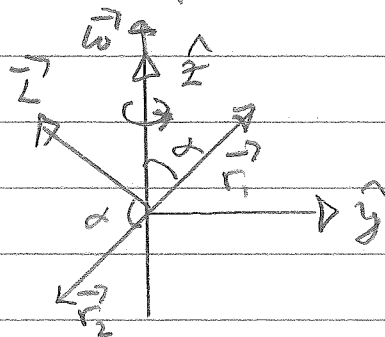
rotations about
z-axis

$$\begin{pmatrix} L_{x_0} \\ L_{y_0} \\ L_{z_0} \end{pmatrix}_{\text{inertial}} = \begin{pmatrix} C_\alpha & -S_\alpha & 0 \\ S_\alpha & C_\alpha & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0 \\ -C_\alpha \\ S_\alpha \end{pmatrix} \left(\frac{S_\alpha m\omega l^2}{2} \right)$$

ωt body

Right-handed rotation of coordinate

Body frame:
axes correspond
between frames @ $t=0$



$$\vec{r}_1 = \frac{l}{2} (S_\alpha \hat{y} + C_\alpha \hat{z})$$

$$\vec{v}_1 = \vec{\omega} \times \vec{r}_1 = \frac{l\omega}{2} S_\alpha (\hat{z} \times \hat{y}) = -\frac{l\omega}{2} S_\alpha \hat{x}$$

$$\begin{aligned} \vec{L} &= 2m \vec{r}_1 \times \vec{v}_1 = 2m \left(\frac{l}{2} \right)^2 \omega (-S_\alpha) (S_\alpha \hat{y} \times \hat{x} + C_\alpha \hat{z} \times \hat{x}) \\ &= \frac{m l^2 \omega}{2} S_\alpha (-C_\alpha \hat{y} + S_\alpha \hat{z}) \end{aligned}$$

$$\vec{L} \xrightarrow{\text{body}} \begin{pmatrix} 0 \\ -C_\alpha \\ S_\alpha \end{pmatrix} \left(\frac{S_\alpha m\omega l^2}{2} \right)$$

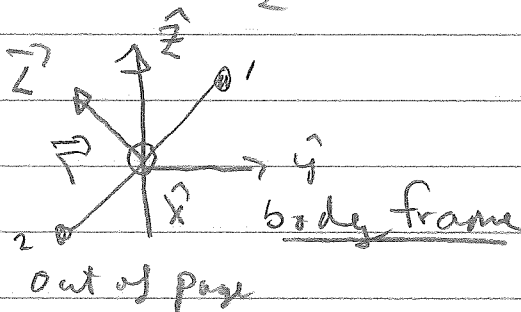
body

$$\text{Torque } \vec{\Gamma} = \left(\frac{d\vec{L}}{dt} \right)_{\text{inertial}} = \vec{\omega} \times \vec{L}$$

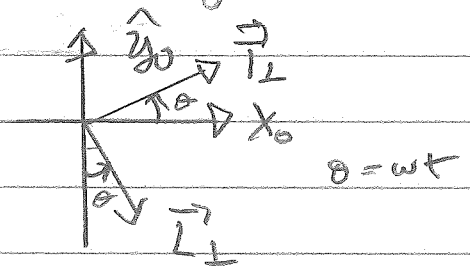
$$= \frac{m\omega^2 l^2}{2} S_x C_x \left[\cos \omega t \hat{x}_0 + \sin \omega t \hat{y}_0 \right]$$

$$= \omega \hat{z} \times \left[\frac{m l^2 \omega}{2} S_x (-C_x \hat{x} + S_x \hat{z}) \right]$$

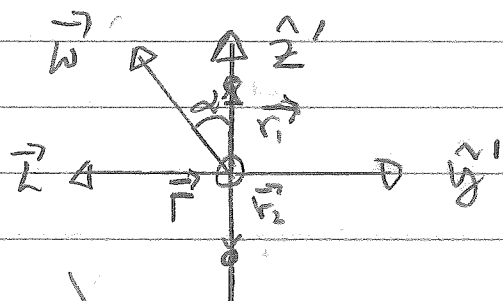
$$= \frac{m\omega^2 l^2}{2} S_x C_x \hat{x}$$



Looking down \hat{z}_0 axis
in inertial frame:



No reason to choose body frame with $\hat{z} \parallel \hat{z}_0$. Much simpler to make \bar{I} diagonal.



$$\vec{\omega}' = \begin{pmatrix} 0 \\ -\sin \alpha \\ \cos \alpha \end{pmatrix} \text{ 'basis } \quad \bar{I}' = \frac{m l^2}{2} \text{diag}(1, 1, 0)$$

$$\vec{L}' = \bar{I}' \cdot \vec{\omega}' = \omega \frac{m l^2}{2} S_x (-\hat{y}')$$

$$\vec{\Gamma}' = \vec{\omega}' \times \vec{L}' = \omega^2 \frac{m l^2}{2} S_x C_x \hat{x}'$$

Principal Axes Euler, 1750

For any rigid body, \bar{I} can be made diagonal by suitable choices of axes.
(math - real, symmetric matrix)

$$\bar{I} = \text{diag}(I_1, I_2, I_3) \quad (\text{single subscript})$$

or λ_i

I_i called principal moments
axes called principal axes.

for $\vec{\omega}$ along principal axes, say $\vec{\omega} = (\omega, 0, 0)$

$$\vec{L} = \bar{I} \vec{\omega}, \quad \vec{\omega} \times \vec{L} = 0 \quad \text{Torque is zero}$$

\vec{L} fixed direction in inertial frame

Finding Principal Axes (diagonalize matrix)

3 Principal axes \hat{w}_p , $\vec{L} = \bar{I} \cdot \hat{w}_p = I_p \hat{w}_p$

or

$$(\bar{I} - I_p \bar{1}) \cdot \hat{w}_p = 0$$

↑ 3x3 unit matrix $(\bar{1})_{ij} = \delta_{ij}$

Solve characteristic (eigenvalue) equation

$$\det | I_{ij} - I_p \delta_{ij} | = 0$$

Cubic, 3 real roots (see Appendix)

Once \bar{I}_p are known,

$$(\bar{I} - \bar{I}_p \bar{I}) \cdot \hat{w}_p = 0$$

gives 2 unique equations (since $|\hat{w}_p|^2 = 1$)

Relation to rotation Matrices

Find rotation \bar{R} that diagonalizes \bar{I} .

$$\bar{I}' = \bar{R} \cdot \bar{I} \cdot \bar{R}' \quad \text{or} \quad \bar{I}' \cdot \bar{R} = \bar{R} \cdot \bar{I}$$

$$\bar{R} \cdot \bar{I} - \bar{I}' \cdot \bar{R} = 0 \quad (*)$$

$$(\bar{R} \cdot \bar{I})_{ij} = \sum_k R_{ik} \bar{I}_{kj}$$

$$(\bar{I}' \cdot \bar{R})_{ij} = \sum_k \bar{I}'_{ik} R_{kj} = \bar{I}'_{ij}; \quad R_{ij} = \sum_k \bar{I}'_{ik} \delta_{kj} R_{kj}$$

So in component form eq. (*) is

$$\sum_k (\bar{I}_{kj} - \bar{I}'_{ik} \delta_{kj}) R_{ik} = 0$$

same secular equation with $R_{ik} = (\hat{w}_i)_k$
 \uparrow
 row index

\hat{w}_p vectors as rows of matrix

$$\bar{R} = \begin{pmatrix} w_{1x} & w_{1y} & w_{1z} \\ w_{2x} & w_{2y} & w_{2z} \\ w_{3x} & w_{3y} & w_{3z} \end{pmatrix}$$

In practice, rarely need to use the rotation matrix

Example: thin plate "lamina"
from Latin "thin sheet of material"

On homework, general form of lamina is

$$\bar{I}_{\text{lamina}} = \begin{pmatrix} A & -C & 0 \\ -C & B & 0 \\ 0 & 0 & A+B \end{pmatrix}$$

take $\bar{I} = A \begin{pmatrix} 1 & -\frac{1}{2} & | & 0 \\ -\frac{1}{2} & 1 & | & 0 \\ 0 & 0 & | & 2 \end{pmatrix}$

2x2 eigenvalue equation

$$A \begin{pmatrix} 1 & -\frac{1}{2} \\ -\frac{1}{2} & 1 \end{pmatrix} \vec{w} = \lambda \vec{w}$$

$$\det \begin{vmatrix} 1-\lambda & -\frac{1}{2} \\ -\frac{1}{2} & 1-\lambda \end{vmatrix} = 0$$

$$(1-\lambda)^2 - \frac{1}{4} = 0$$

$$1-\lambda = \pm \frac{1}{2}$$

$$\lambda = \frac{1}{2}, \frac{3}{2}$$

$$\lambda = \frac{1}{2} \begin{pmatrix} 1 - \frac{1}{2} & -\frac{1}{2} \\ -\frac{1}{2} & 1 - \frac{1}{2} \end{pmatrix} \begin{pmatrix} w_1 \\ w_2 \end{pmatrix} = 0$$

$$\frac{1}{2} w_1 - \frac{1}{2} w_2 = 0 \quad (2^{\text{nd}} \text{ eq. redundant})$$

$$w_1 = w_2$$

$$\hat{w}_{\frac{1}{2}} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\lambda = \frac{3}{2} \begin{pmatrix} 1 - \frac{3}{2} & -\frac{1}{2} \\ -\frac{1}{2} & 1 - \frac{3}{2} \end{pmatrix} \begin{pmatrix} w_1 \\ w_2 \end{pmatrix} = 0$$

$$\hat{w}_{\frac{3}{2}} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -1 \end{pmatrix}$$

note $\hat{w}_{\frac{1}{2}} \cdot \hat{w}_{\frac{3}{2}} = 0$

check $\bar{I}' = \bar{R} \bar{I} \bar{R}^{-1}$

$$\bar{R} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 & -1 \\ 1 & 1 \end{pmatrix} \quad \begin{array}{l} \lambda = \frac{3}{2} \text{ row} \\ \lambda = \frac{1}{2} \text{ row} \end{array}$$

$$\frac{1}{2} \begin{pmatrix} 1 & -1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} 1 & -\frac{1}{2} \\ -\frac{1}{2} & 1 \end{pmatrix} \begin{pmatrix} 1 & -1 \\ -1 & 1 \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} 1 & -1 \\ 1 & 1 \end{pmatrix} \begin{pmatrix} \frac{3}{2} & \frac{1}{2} \\ -\frac{3}{2} & \frac{1}{2} \end{pmatrix} = \begin{pmatrix} \frac{3}{2} & 0 \\ 0 & \frac{1}{2} \end{pmatrix}$$